



SOLUTIONS & COLLIGATIVE PROPERTIES

Concentration Terms

- i. A or 1 = Solvent,
B or 2 = Solute,
C or 3 = Solution

- ii. W = Weight,
V = Volume
d = density

iii. $W_C = W_A + W_B$

iv. $W_A = W_1 = \text{Weight of solvent}$

☆ Concentration of Solution

- i. **Conc. of Solution** = Conc. of Solute

$$= \frac{\text{no - of moles of solute}}{\text{Volume of solution}}$$

- ii. Methods of expressing concentration of solution.

$$M, N, m, \% \frac{W}{W}, \% \frac{W}{V}, X, \text{PPb}, \text{PPm}, \text{strength}$$

Molarity and Normality (A = Solvent, B = Solute, C = Solution)

☆ Molarity (M)

i. $M = \frac{n_B}{V_C \text{ lt}}$

ii. $M = \frac{W_B}{M.W_B} \times \frac{1}{V_C \text{ (lt)}}$

iii. $M = \frac{W_B}{M.W_B} \times \frac{1000}{V_C \text{ (M)}}$

iv. $M = \frac{\text{no - of solute molecules}}{N_A} \times \frac{1000}{V_C \text{ ml.}}$

v. no - of moles of solute = $M \times V_C \text{ (lt)}$

vi. no - of millimoles of solute = $M \times V_C \text{ (ml)}$

vii. Wt of solute = $W_B = n_B \times M.W_B$

viii. 1 Molar = 1 M = 1 mol/lt

Decimolar = 0.1 M = M/10

Centimolar = 0.01 M = M/100

Millimolar = 0.001 M = M/1000

Semi molar = 0.5 M = M/2

Penti molar = 0.2 M = M/5

Deca molar = 10 M.

☆ Normality (N)

i. $N = \left(\frac{\text{no - of gm. eq of solute}}{\text{Vol. of solute (lt)}} \right)$

ii. $N = \frac{W_B}{E_B} \times \frac{1000}{V_C \text{ ml}}$

(E = Gram equivalent weight)

iii. no - of gm. eq of solute = $N \times V_C \text{ (lt)}$

iv. No - of millieq. of solute = $N \times V_C \text{ (ml)}$

v. Unit : gm. eq./lt

Note : First find molarity then find normality

$$N = M \times V.f$$

Molality, Mole Fraction and Strength (A = Solvent, B = Solute, C = Solution)

☆ Molality (m)

i. $m = \frac{n_B}{W_A \text{ (kg)}}$

ii. $m = \frac{n_B}{M.W_B} \times \frac{100}{W_A \text{ (gm)}}$

iii. 1 molal = 1 m = 1 mole/kg

Decimolal = 0.1 m = m/10

☆ Mole fraction (x)

- i. If a mixture or solution contains three components of moles n_1, n_2 & n_3 .

- ii. If x_1, x_2, x_3 are mole fraction of each components.

- iii. Let $N = n_1 + n_2 + n_3 = \text{Total moles}$

iv. $x_1 = \frac{n_1}{N}, x_2 = \frac{n_2}{N}, x_3 = \frac{n_3}{N}$

v. $x_1 + x_2 + x_3 = 1$

∴ Sum case of mole fraction on = 1

- vi. In case of binary solution

$$x_A = \frac{n_A}{n_A + n_B}; \quad x_B = \frac{n_B}{n_A + n_B}$$

$$x_A + x_B = 1$$

☆ Strength in gm/lt (S) :

i. $S = \frac{W_B \text{ (gm)}}{V_A \text{ lt}}$

ii. $W_B = (S) (V_C \text{ lt})$

Percentage, PPM, PPb, PPT (A = Solvent, B = Solute, C = Solution)

i. %by weight (% W/W)

$$\% \frac{W}{W} = \frac{W_B}{W_C} \times 100$$

$$(W_C = W_A + W_B)$$

ii. % Wt by Vol. %W/V or W/V%

$$\% \frac{W}{V} = \frac{W_B}{V_C} \times 100$$

iii. % Vol. by Vol. (%V/V)

- It is applicable for **liquid in liquid** type of solution.
- Let V_A, V_B, V_C = Vol. of solvent, solute and solution.
- If $V_C = V_A + V_B$ = Ideal sol.
 $V_C < V_A + V_B$ = Non Ideal -ve deviation
 $V_C > V_A + V_B$ = Non Ideal +ve deviation.

$$\% \frac{V}{V} = \frac{V_B}{V_C} \times 100$$

☆ PPM, PPb, PPT

i. These are used to express the conc. of very dilute solution and conc. of gaseous pollutant.

ii. In case of solids in liquid solution.

- no - of PPM = $\frac{W_B}{W_C} \times 10^6$
- no - of PPb = $\frac{W_B}{W_C} \times 10^9$
- no - of PPT = $\frac{W_B}{W_C} \times 10^{12}$
- Ex : 100 PPM Sugar solution means 100 gm of sugar present in 10^6 gm of solution.

iii. In case of gas in gas solution.

$$\text{no - of PPM} = \frac{V_B}{V_C} \times 10^6$$

Ex : 100 PPM of CO_2 in air is 100 ml of CO_2 present in every 10^6 ml of air mixture.

Interconversion of Concentration Terms (A = Solvent, B = Solute, C = Solution)

$$\text{i. } M = \frac{\% \frac{W}{V} \times 10}{M.W_B}$$

$$\text{ii. } M = \frac{\% \frac{W}{W} \times d_C \times 10}{M.W_B}$$

$$\text{iii. } M = \frac{S(\text{gm/lit})}{M.W_B}$$

$$\text{iv. } N = M \times V. f$$

$$\text{v. } S(\text{gm/lit}) = \% \frac{W}{V} \times 10$$

$$\text{vi. } \% \frac{W}{V} = \% \frac{W}{W} \times d_C$$

vii. In case of binary solution.

$$\bullet X_B = \frac{m}{m + \left(\frac{1000}{M.W_A} \right)} \quad (\text{For any sol.})$$

• In case of aqueous solution.

$$X_B = \frac{m}{m + 55.5}$$

$$\text{viii. } \frac{d_C}{M} = \frac{1}{m} + \frac{M.W_B}{1000} \quad \text{or} \quad m = \frac{1000 \times M}{(1000 \times d) - (M \times M.W_{\text{solute}})}$$

But in case of very dilute solution, $M = m \times d_C$

ix. When % W / W of solute is given

$$m = \frac{\% W / W}{M_2} \times \frac{1000}{(100 - \% w / w)}$$

x. Relation betⁿ molarity & mole fraction

$$M = \frac{X_{\text{Solute}} \times 1000 \times d_c}{(X_{\text{Solute}} \times M.W_{\text{Solute}}) + (X_{\text{Solvent}} \times M.W_{\text{Solvent}})}$$

Note:

- In case of aq. solution or density of solvent ≥ 1
Then concentration of 1 M > 1 ml
- If density of solvent < 1
Then concentration of 1 M < 1 m

Concept of Dilution

i.

Before Dilution (B / D)	After Dilution (A / D)
M_1	M_2
N_1	N_2
V_1	V_2

- ii. On dilution, amount of **solute constant**
 $M \times V = \text{no of moles of solute} = \text{constant}$
 $N \times V = \text{no of gm.eq of solute} = \text{constant}$

iii.

$$\boxed{M_1 V_1 = N_2 V_2}$$

$$\boxed{N_1 V_1 = N_2 V_2}$$

- iv. $V_2 - V_1 = \text{volume of solvent added for dilution.}$

v.

$$\frac{V_2}{V_1} = \frac{M_1}{M_2} = \frac{N_1}{N_2} = \text{N.T.D.}$$

(N. T. D = No of time of dilution)

Mixing of Solutions of non reacting solutes

i.

Sol ⁿ 1	Sol ⁿ 2
M_1	N_2
N_1	N_2
V_1	V_2

- ii. If $M_R, N_R = \text{Resultant molarity and normality of mixture of solution 1 and 2.}$

iii.

$$M_R = \frac{\text{Total moles of solute}}{\text{Total Vol. of solution}}$$

$$M_R = \frac{M_1 V_1 + M_2 V_2}{V_1 + V_2}$$

iv.

$$N_R = \frac{\text{Total gm. eq of solution}}{\text{Total Vol. of sol.}}$$

$$N_R = \frac{N_1 V_1 + N_2 V_2}{V_1 + V_2}$$

- v. If the above two solutions are mixed and then diluted to **vol. (V)** then

- $M_R = \frac{M_1 V_1 + M_2 V_2}{V}$

- $N_R = \frac{N_1 V_1 + N_2 V_2}{V}$

- Volume of H_2O added for dilution
 $= V - (V_1 + V_2)$

Mixing of Solutions of reacting solutes

☆ Mixing of Solutions of reacting solutes

- i. Ex : of reacting solutes

- Acid – Base
- Oxidising agent + Reducing agent

- ii. Consider of mixture of Acid and Base

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Acid	Base
N_a	N_b
V_a	V_b

- If $N_a V_a > N_b V_b$, then

$$N_R = [H^+] = \left(\frac{N_a V_a - N_b V_b}{N_b + V_b} \right)$$

- If $N_b V_b > N_a V_a$, then

$N_R = \text{Resultant Normality of unreacted (U.R) Base.}$

$$N_R = [OH^-] = \left(\frac{N_b V_b - N_a V_a}{V_a + V_b} \right) \quad M_R = \left(\frac{N_R}{V.f} \right)$$

- If $N_a V_a = N_b V_b$, then

Nature of solution = neutral

$N_R = \text{Resultant normality of solution}$
 $= \text{normality of salt formed}$

$$N_R = \left(\frac{\text{no. of eq. of salt formed}}{\text{Total volume}} \right) = \frac{x}{V_a + V_b}$$

no of eq. of salt formed = $x = N_a V_a = N_b V_b$

Henry's Law

i. Statement :

Solubility of gas \propto Partial Pressure of gas

ii. Let S = Molar solubility mole/lit

$$S = \frac{n(g)}{V_c l t}$$

$n(g)$ = no of moles of gas in dissolved state.

iii. $P_{(g)} = K_H S_{(g)}$

K_H = Henry's constant.

iv. The value of K_H depends on nature of gas, nature of solvent, temp and pressure.

- v. Solubility of gas $\propto \frac{1}{K_H}$
- \propto I. M. F
 - $\propto T_c$
 - \propto Liquification of gas
 - $\propto \frac{a}{b}$ (a, b = vanderwaal const.)
 - \propto Pressure of gas
 - $\propto \frac{1}{\text{Temp.}}$

v. The Henry's formula depends on unit of K_H

Step I : Check the unit of K_H

Step II : Apply the related formula.

Unit of K_H	Henry's Formula
mole $l t^{-1} atm^{-1}$	$S_{(g)} = K_H \cdot P_{(g)}$
atm $l t mole^{-1}$	$P_{(g)} = K_H \cdot S_{(g)}$
atm $g m^{-1}$	$P_{(g)} = K_H \cdot m_{(g)}$
atm $^{-1}$	$x_{(g)} = K_H \cdot P_{(g)}$
gm atm^{-1}	$m_{(g)} = K_H \cdot P_{(g)}$

vi. Effect of temp. on Solubility of solid in liquid

- Solubility $\propto \frac{1}{\text{Temp.}}$ (Exothermic dissolution)
Ex.: Na_2SO_4 , Ce_2SO_4
- Solubility \propto Temp. (Endothermic dissolution)
Ex.: $NH_4 NO_3$, $NaNO_3$, KNO_3 , KBr

- Solubility of $NaCl$, KCl & $NaBr$ increases slightly with increase in temperature.
- The salt which are more soluble at high temperature are recrystallised first
- Crystallisation of



Colligative Properties (C. P.)

- i. C. P. are the properties of dilute solution containing non – volatile solute (N.V. S)
- ii. The values of C. P. depends on No. of solute particles but do not depends on nature of solute particles.
- iii. The solute particles may be covalent molecule or ions
- eg. 2 mole glucose and 1 mol $NaCl$ have same no of solute particles.
- iv. C. P. are used to calculate the molecular weight of non volatile solute.
- v. C. P. are
 - a) RLVP
 - b) ΔT_b
 - c) ΔT_f
 - d) π
- vi. On addition of N.V. S to volatile solvent, then V. P of solvent decreases. This is called lowering of V.P.
 $P^\circ =$ V. P. of solvent
 $P^s =$ V. P. of solvent + N. V. S
 $=$ V. P. of solution
- vii. $P^\circ > P^s \Rightarrow P^\circ - P^s > 0$ (+ve)
- viii. Lowering in V. P = $\Delta P = P^\circ - P^s$

ix. R. L. V. P. = $\frac{P^\circ - P^s}{P^\circ}$

x. % Lowering in V.P. = $\frac{P^\circ - P^s}{P^\circ} \times 100$

Relative lowering in vapour pressure (RLVP)

vi. Raoult's law for a solution containing N.V.S.

Statement of Raoult's law

$$\frac{P^\circ - P^S}{P^\circ} = i \cdot x_B$$

$$\frac{P^\circ - P^S}{P^\circ} = i \cdot \frac{W_B}{M \cdot W_B} \times \frac{M \cdot W_A}{W_A}$$

vii. Ostwald - walker method to find RLVP

- On passing dry air into solution bulb and then into solvent bulb.
- Then dry air absorbs the water vapour of the solution and solvent bulb.
- Then there is loss in weight of solution & solvent bulb.
- W_1 = Loss in weight of solution bulb.
- W_2 = Loss in weight of solvent bulb.
- W_3 = Gain in weight of CaCl_2 tube.

$$W_3 = W_1 + W_2$$

$$\frac{P^\circ - P^S}{P^\circ} = \left(\frac{W_2}{W_1 + W_2} \right) = \frac{W_2}{W_3}$$

viii. Raoult's Law for a Mixture of volatile liquids

- Consider mixture two Volatile liquids (A) & (B)
- In the mixture of A & B.**

a) In solution phase (Raoult's Law) :

$$P_A = P_A^\circ X_A, P_B = P_B^\circ X_B$$

$$\therefore P_T = P_A^\circ X_A + P_B^\circ X_B$$

$$P_T = P_A + P_B$$

b) In vapour phase (Dalton's Law) :

$$P_A = P_T \cdot Y_A = P_A^\circ X_A$$

$$P_B = P_T \cdot Y_B = P_B^\circ X_B$$

- P_A, P_B = Parital pressure of A & B
- P_A°, P_B° = V.P. of pure component of A & B
- X_A, X_B = Mole fraction of A & B in liq. state
- Y_A, Y_B = Mole fraction of A & B in Vap. state

Ideal & Non-Ideal solution

Ideal	Non ideal +ve deviations	Non ideal -ve deviations
It Obeys Raoult's law. $\Delta V_{\text{mix}} = 0, \Delta H_{\text{mix}} = 0$ $\Delta S_{\text{mix}} > 0, \Delta G < 0$ Attractions of A-A = B-B = A-B $P_A = P_A^\circ X_A$ and $P_B = P_B^\circ X_B$	It Do not Obeys Raoult's law. $\Delta V_{\text{mix}} > 0, \Delta H_{\text{mix}} > 0$ $\Delta S_{\text{mix}} > 0, \Delta G < 0$ Attractions of A-B < Avg. of B-B & A-A $P_A > P_A^\circ X_A$ and $P_B > P_B^\circ X_B$	It Do not Obeys Raoult's law. $\Delta V_{\text{mix}} < 0, \Delta H_{\text{mix}} < 0$ $\Delta S_{\text{mix}} > 0, \Delta G < 0$ Attractions of A-B > Avg. of B-B & A-A $P_A < P_A^\circ X_A$ and $P_B < P_B^\circ X_B$
Ex. a. Methanol + ethanol b. Ethyl bromide + methyl bromide c. Benzene & toluene d. n-heptane + N-Hexane e. CCl_4 + benzene	Ex. a. Acetone + Ethanol b. Acetone + CS_2 c. Acetone + C_6H_6 d. $\text{H}_2\text{O} + \text{CH}_3\text{OH}$ e. $\text{H}_2\text{O} + \text{C}_2\text{H}_5\text{OH}$ f. CCl_4 + toluene g. $\text{CCl}_4 + \text{CHCl}_3$ h. $\text{CCl}_4 + \text{CH}_3\text{OH}$	Ex. a. Acetone + Aniline b. Acetone + CHCl_3 c. $\text{CH}_3\text{OH} + \text{CH}_3\text{COOH}$ d. $\text{H}_2\text{O} + \text{HNO}_3$ e. $\text{CHCl}_3 + \text{C}_2\text{H}_5\text{O}-\text{C}_2\text{H}_5$ f. $\text{H}_2\text{O} + \text{HCl}$ g. $\text{CH}_3\text{COOH} + \text{Pyridine}$ h. $\text{CHCl}_3 +$

Azeotropic Mixture

- Azeotrope is a binary mixture having same composition in **liquid & vapour phase & boil** at a constant temperature.
- These mixtures are **formed by only Non-ideal** solutions.

They are of two types

- Minimum boiling azeotrope** are formed by the solutions with show **positive deviation** from **Raoult's law**.
 - Maximum boiling azeotrope** are formed by the solutions with how **negative deviation** from **Raoult's law**.
- Components of azeotropic mixture **can not** be separated by **fractional distillations**.

Note:

1. V.P. Do not depend on

- Amount of liquid
- Size of vessel
- Surface area of liquid

2. V.P. Depend on

- Nature of liquid
- Temp.

Abnormal C. P. & Van't hoff factor(i)

i.
$$i = \frac{A.C.P}{N.C.P}$$

ii.
$$i = \left(\frac{\text{no - of Solute partices After Association or Dissociation}}{\text{no - of Solute partices Before Association Dissociation}} \right)$$

iii.
$$i = \frac{(M.W)_T}{(M.W)_E}$$

$(M.W)_T$ = Theoretical or calculated or actual **M.W**

$(M.W)_E$ = Experimented or observed **M. W**

A.C.P. = Abnormal colligative property or observed colligative property.

N.C.P. = Normal colligative property or calculated colligative property

iv. In case of dissociation

$$\alpha = \frac{i-1}{n-1}$$

n = no – of partices formed from **1** particles of solute.

v. In case of Association.

$$\alpha = \frac{1-i}{1-\frac{1}{n}}$$

n = no–of particle associatiate to from one particle.

Boiling point elevation(ΔT_b)

- On addition of **N.V.S** to a volatile solvent, then **V. P.** of volatile Solvent, decreases, Hence **B.P** of Solvent Increases. This is called **B.P** elevation (ΔT_b)

- $$\Delta T_b = i \cdot K_b \cdot m$$

K_b = Ebulliosopic or mole B.P elevation constant.

- $$\Delta T_b = T_s - T_0$$

T_0 = **B.P** of solvent

T_s = **B.P** of solvent + **N.V.S** = **B.P.** of solution

- Unit of $K_b = ^\circ\text{C kg mole}^{-1}$

$$= K \cdot \text{kg mol}^{-1}$$

$$= K \text{ mol}^{-1}$$

- **B. P.** of liquids $\propto (P_2 - P_1)$

P_1 = Vapour Pressure of liquid

P_2 = Atmospheric Pressure

- **B. P.** of solution \propto concentration of solute.

- **B. P.** of solution $\propto \Delta T_b$.

$$K_b = \frac{RT_0^2 M_A}{1000 \times \Delta H_{\text{vap}}}$$

$$K_b = \frac{RT_0^2 M_A}{1000 \times \Delta H_{\text{vap}}}$$

- ΔH_{vap} = Heat of Vapourisation = amount of heat required to vapourise **1** mole of lig. at its **B.P**

- L_{vap} = Latent heat of Vapourisation

= amount of heat required to vapourise **1** mole of solvent.

- $$\Delta H_{\text{vap}} = L_{\text{vap}} \times M_A$$

T_0 = **B. P** of solvent.

R = Gas constant.

Freezing point Depression (ΔT_f)

i. On Addition of N.V.S. to a volatile solvent, F. P. of Solvent decreases. This is called F. P. depression.

ii.
$$\Delta T_f = T_o^f - T_s^f$$

$T_o^f = \text{F. P. of pure Solvent}$

$T_s^f = \text{F. P. of pure Solvent} + \text{N.V. S}$
 $= \text{F. P. of Solution.}$

iii.
$$\Delta T_f = i \cdot K_f \cdot m$$

$K_f = \text{Cryoscopic const. or molal F. P. dep. const.}$

iv.
$$\text{F.P of liquid} \propto \text{its V.P}$$

v. Among two or many solutions

$\text{F. P. of solution} \propto \text{V. P} \propto \frac{1}{\text{Conc of solution}}$

vi. $\Delta T_f \propto \text{Conc of solute.}$

vii.
$$K_f = \frac{R \cdot (T_f^0)^2 M_A}{1000 \times \Delta H_{\text{Fus}}}$$

$$K_f = \frac{R \cdot (T_f^0)^2}{1000 \times L_{\text{Fus}}}$$

$T_f^0 = \text{F. P. of solvent.}$

$M_A = \text{M. W of solvent in gm.}$

viii. $\Delta H_{\text{Fus}} = \text{amount of heat required to fuse one mole solid to liquid at its melting point.}$

ix. $L_{\text{Fus}} = \text{Latent heat of Fusion} = \text{Amount of heat required to fuse 1 gm of solid to liquid at its M.P.}$

$$\Delta H_{\text{Fus}} = L_{\text{vap}} \times M.W_A$$

Osmotic Pressure (π)

i. O. P = Pressure applied from the solution side to stop osmotic.

ii. If the pressure applied is more than O. P, then solvent flow from solution to pur. solvent. This is called reverse Osmosis (R.O)

iii. $\pi = i M R T$

iv. O. P of Dilution :

B/D	A/D
π_1	π_2
V_1	V_2

$$\pi_1 V_1 = \pi_2 V_2$$

• $V_2 - V_1 = \text{Volume of water added for Dilution.}$

v. O. P. of mixing for Non reacting solute :

Sol-1	Sol-1	Mixture
π_1	π_2	$\pi_R \neq \pi_1 + \pi_2$
V_1	V_2	$V = V_1 + V_2$

$$\pi_R = \frac{\pi_1 V_1 + \pi_2 V_2}{V}$$

• If molarities of solution are given :

Sol-1	Sol-1	Mixture
M_1	M_2	
V_1	V_2	$M_R = ?$
i_1	i_2	

$$M_R = \left(\frac{i_1 M_1 V_1 + i_2 M_2 V_2}{V_1 + V_2} \right)$$

$$\pi = (M_R) (R) (T)$$

vi. Abe Nollet Experiment :

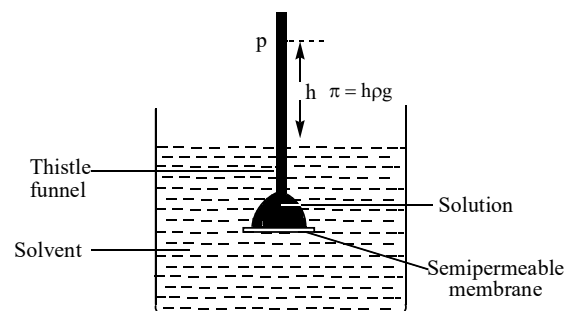
$$\pi = h d g$$

$h = \text{Rise in height of liquid}$

$d = \text{Density of solution}$

$g = \text{Acceleration due to gravity.}$

• This experiment do not calculate, accurate osmotic pressure because density of solution changes wrt. height.



Phenomenon of osmosis

Colligative Properties

Solute

C.P. of dilute solution

- ∞ Number of solute particles
- ∞ Number of molecules
- ∞ Number of ions
- ∞ Number of moles of solute
- ∞ Mole fraction of solute
- ∞ do not depends on nature of solute

Incase of Non Electrolyte
i.e. glucose, sucrose

Incase of Electrolyte
Abnormal C.P.

Neither Associate Nor dissociate
i (Van't of Hoff factor) = 1
Normal Colligative Properties

Association

Dissociation

a) Relative lowering in vapour pressure of solvent

$$\frac{P_0 - P_s}{P_0} = i \frac{n}{n+N}$$

b) Elevation in boiling point (ΔT_b) of solvent

$$\Delta T_b = i K_b m$$

c) Depression in freezing point (ΔT_f) of solvent

$$\Delta T_f = i K_f m$$

d) Osmotic pressure (π or P) of solution

$$\pi = i CST$$

$$I = 1 + \left(\frac{1}{n} - 1\right) \beta$$

$$i < 1$$
 where α is degree of association & n number of moles
 e.g. Benzoic acid forming dimer in benzene
 $2A \rightarrow A_2; n = 2$ (Dimer)
 $3A \rightarrow A_3; n = 3$ (Trimer)
 $4A \rightarrow A_4; n = 4$ (Tetramer)
 $5A \rightarrow A_5; n = 5$ (Pentamer)

$$i = 1 + (n - 1) \alpha$$

$$i > 1$$
 where α is degree of dissociation & n number of moles of ions

Strong electrolyte
 $i = n; \alpha = 1$ (100%)

Weak electrolyte
 $i > 1; \text{but } 1 < n$

Strong Acid

Strong Base

Salt

Weak Acid

Weak Base

e.g.
 $H_2SO_4, n = 3, i = 3$
 $H_2SO_4 \rightarrow 2H^+ + SO_4^{2-}$
 $HCl, n = 2, i = 2$

NaOH,
 $n = 2, i = 2$

NaCl
 $n = 2, i = 2$

CH_3COOH
 $i > 1; \text{but } 1 < n$

NH_4OH
 $i > 1; \text{but } 1 < n$

A.B. C.P. < Normal C.P.
 A.B. O.P. < Normal O.P.
 A.B. ΔP < Normal ΔP
 A.B. ΔT_b < Normal ΔT_b
 A.B. ΔT_f < Normal ΔT_f

Dissociation

A.B. C.P. > Normal C.P.
 A.B. O.P. > Normal O.P.
 A.B. ΔP > Normal ΔP
 A.B. ΔT_b > Normal ΔT_b
 A.B. ΔT_f > Normal ΔT_f

Note: $C.P. \propto \frac{1}{\text{Molar Mass}}$

$$i = \frac{\text{Normal molar mass}}{\text{observed molar mass}}$$

$$i = \frac{\text{observed colligative properties}}{\text{Normal colligative properties}}$$